

The EPFL logo is rendered in a bold, red, sans-serif font. The letters 'E', 'P', and 'F' are connected at the top, while the 'L' is separate. The logo is positioned to the right of a vertical red bar that runs down the left side of the slide.

Génie Electrique et Electronique  
Master Program  
Prof. Elison Matioli

A large red rectangular box occupies the right half of the slide. Inside, the course title is written in white, bold, sans-serif font. The text is centered and reads: 'EE-557', 'Semiconductor devices I', and 'Power semiconductor devices' on three separate lines.

# EE-557

## Semiconductor devices I

### Power semiconductor devices

## Outline of the lecture

### Basics of power devices

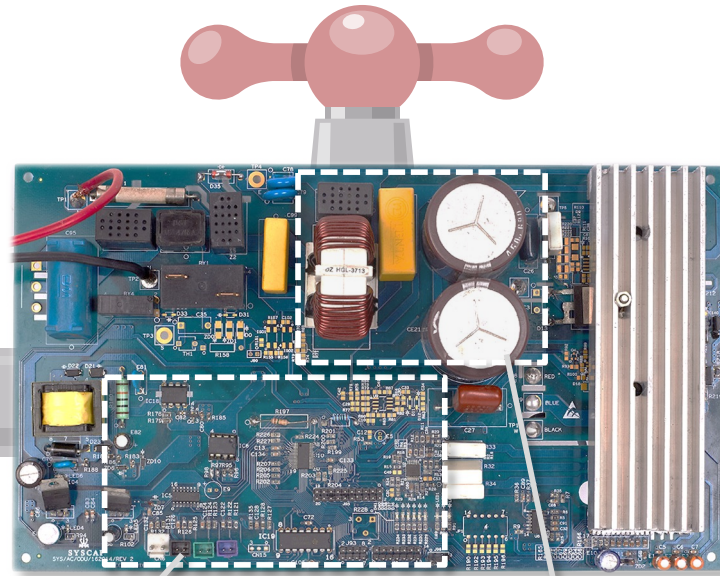
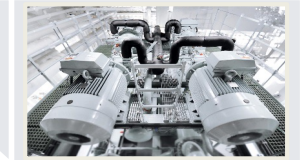
- Baliga's figure of merit
- Power diodes
- Power MOSFETs
- IGBTs

### References:

Chapter 4.2 of Fundamentals of Power Electronics – second edition – Robert W. Erickson and Dragan Maksimović, Kluwer Academic Publishers, 2004

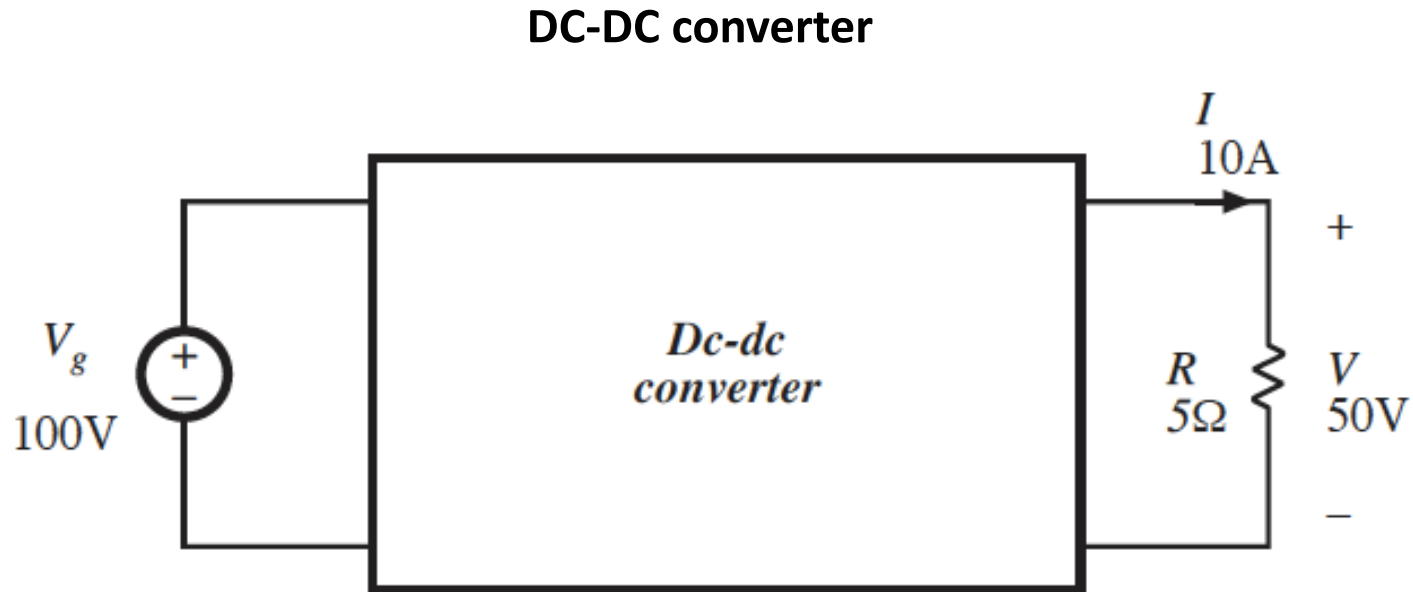
- How can semiconductor devices hold large voltages for power applications?
- How is the voltage related to the semiconductor properties?
- What are the different types of semiconductor power devices?

## Power Electronics



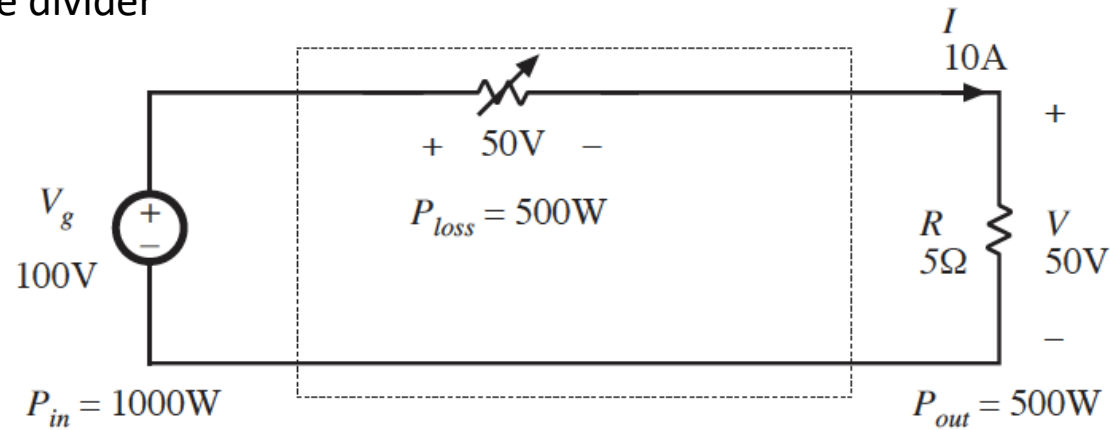
**Semiconductor devices:**  
transistors, diodes, and  
thyristors

**Passive components:**  
capacitors, inductors,  
transformers, etc.

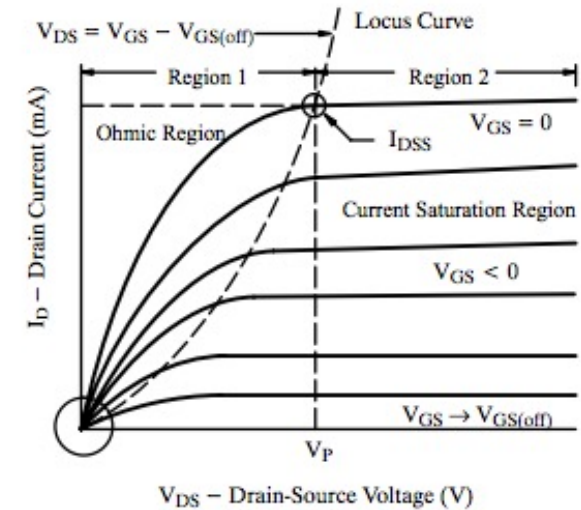
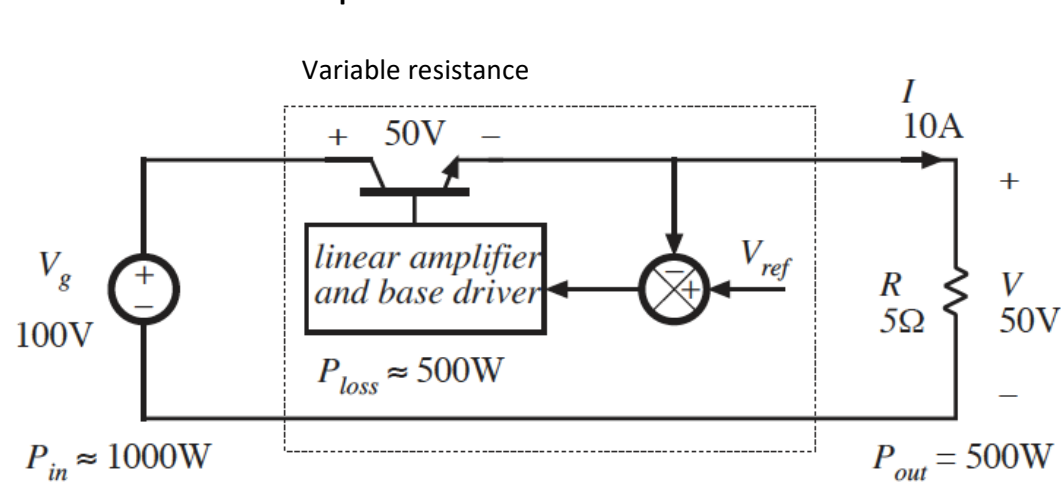


How can such converter be realised?

## Solution 1: voltage divider



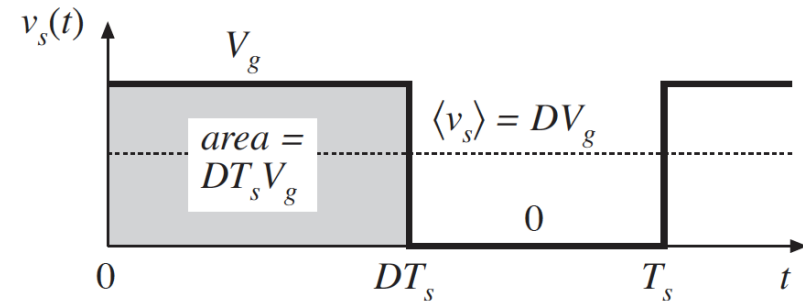
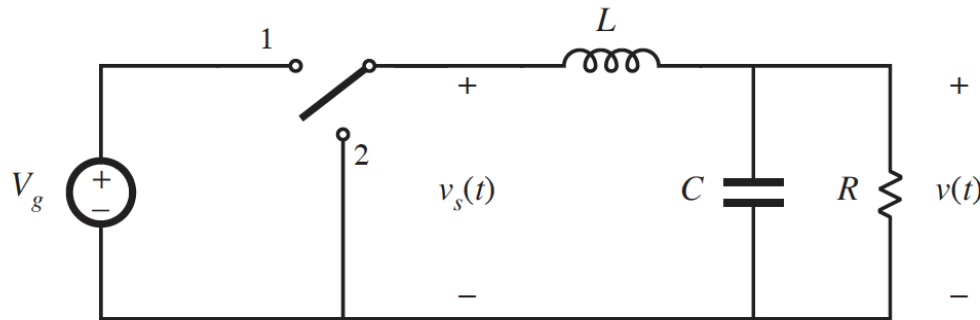
## Solution 2: linear amplifier



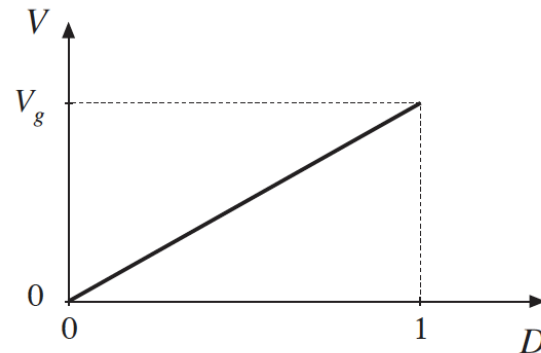
These are very inefficient solutions

## Concept of switching

DC-DC converter (buck converter)



$$v \approx \langle v_s \rangle = DV_g$$



Fourier analysis: Dc component = average value

$$\langle v_s \rangle = \frac{1}{T_s} \int_0^{T_s} v_s(t) dt$$

$$\langle v_s \rangle = \frac{1}{T_s} (DT_s V_g) = DV_g$$

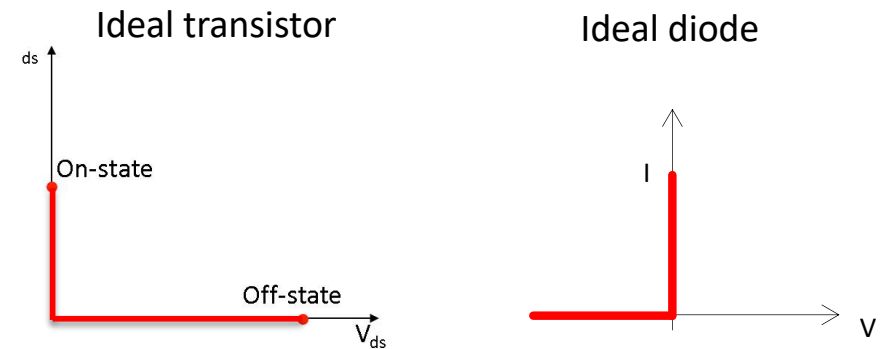
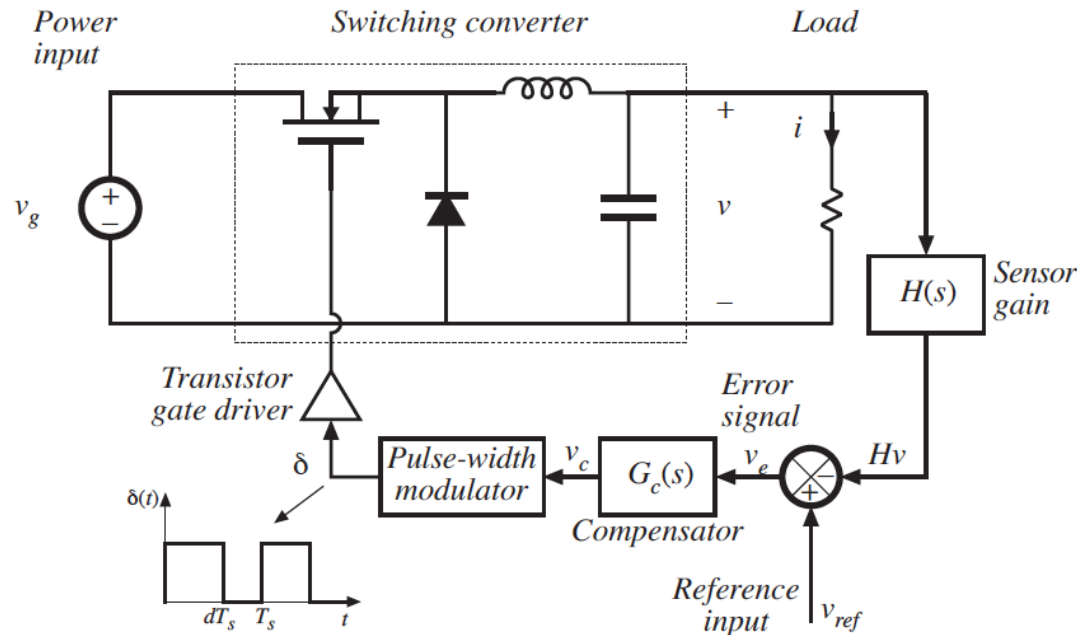
High frequency harmonics are filtered out by the LC filter:

- Cut-off frequency of the LC filter must be much smaller than the switching frequency  $f_0 \ll f_s$

Only DC at the output: This is called a **buck converter**:  $V_{out} = DV_{in}$

## Realization of such circuit:

Power transistors + power diodes + filters + circuit de regulation



Product  $V \times I$  must be as close as possible to zero

Power transistors and diodes are the heart of power converters

They are power switching devices, which:

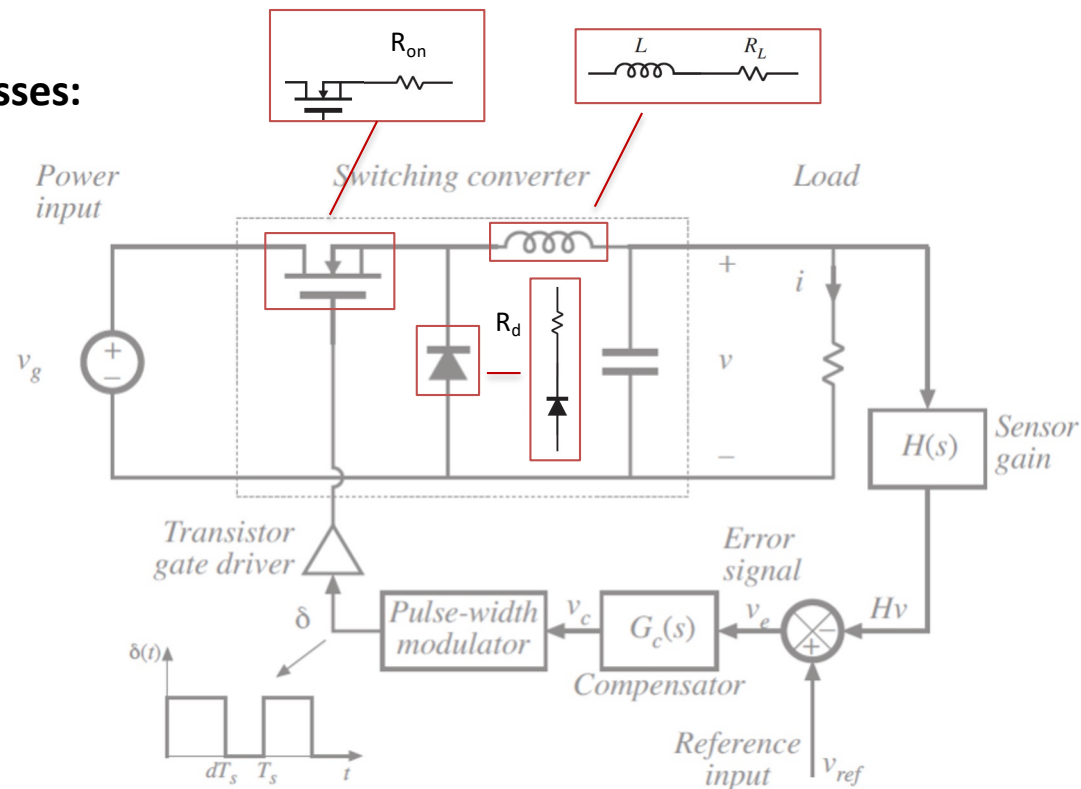
Should **conduct with small losses**, **switch fast** with small losses, **hold large voltages**

Efficient conversion is the goal: **what are the loss mechanisms?**

## Two main loss mechanisms:

1. **Conduction losses:** when devices are conducting
  - Semiconductor forward bias
  - Parasitics: inductances, capacitances, resistances
2. **Switching losses:** when devices are switching

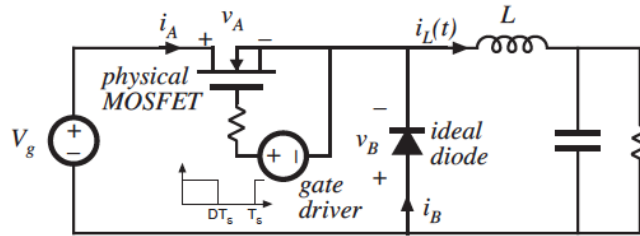
### 1. Conduction losses:



Dissipated power

$$P_{\text{conduction}} = R_{\text{on}} I_{\text{RMS}}^2$$

## 2. Switching losses:



Buck converter example

$$v_B(t) = v_A(t) - V_g \quad \text{transistor turn-off transition}$$

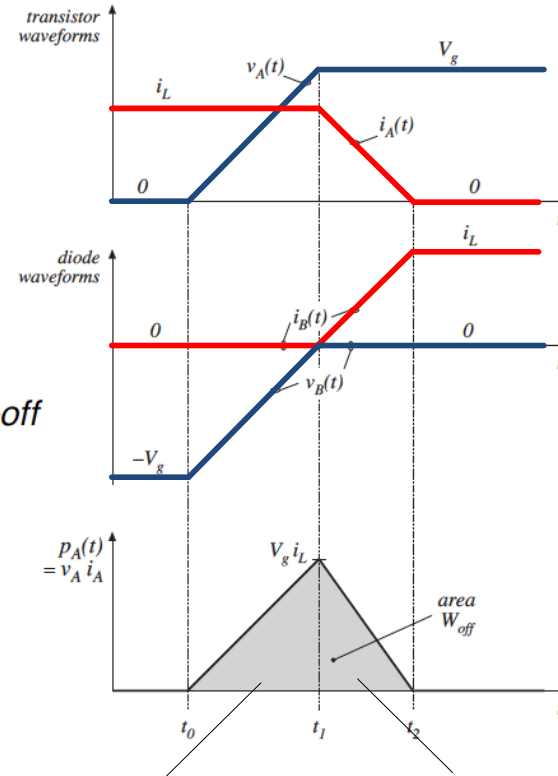
$$i_A(t) + i_B(t) = i_L$$

Energy lost during transistor turn-off transition:

$$W_{off} = \frac{1}{2} V_g i_L (t_2 - t_0)$$

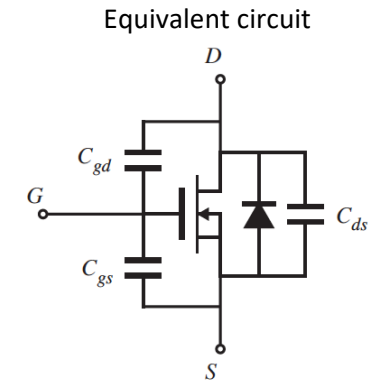
Similar result during transistor turn-on transition.  
Average power loss:

$$P_{sw} = \frac{1}{T_s} \int_{\text{switching transitions}} p_A(t) dt = (W_{on} + W_{off}) f_s$$



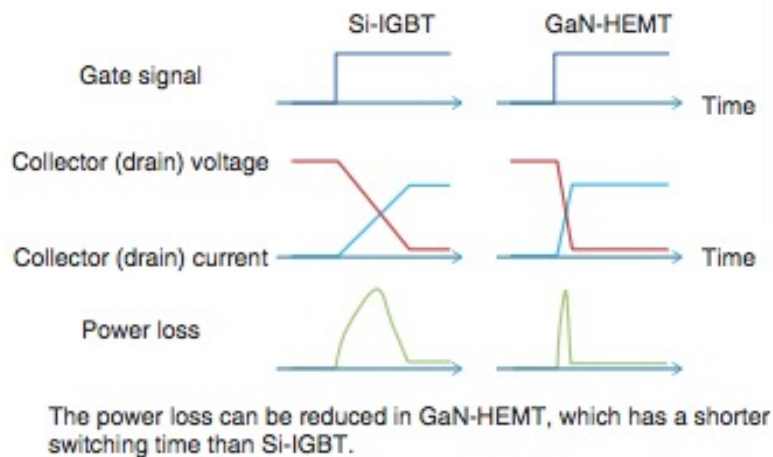
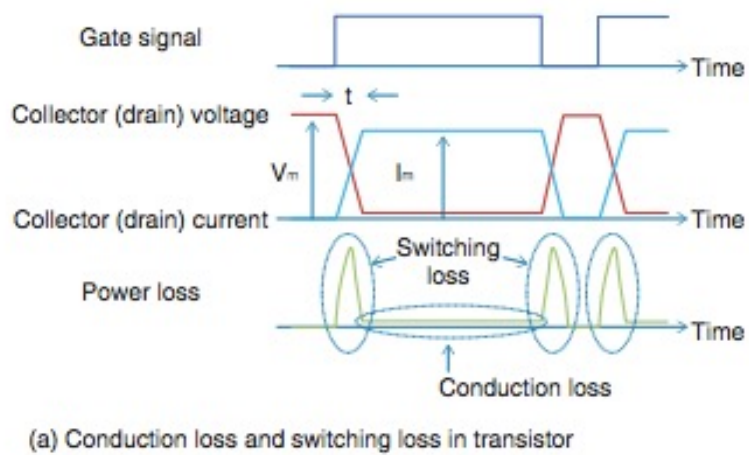
Charging time of  $C_{GD}$

Discharging time of  $C_{GS}$

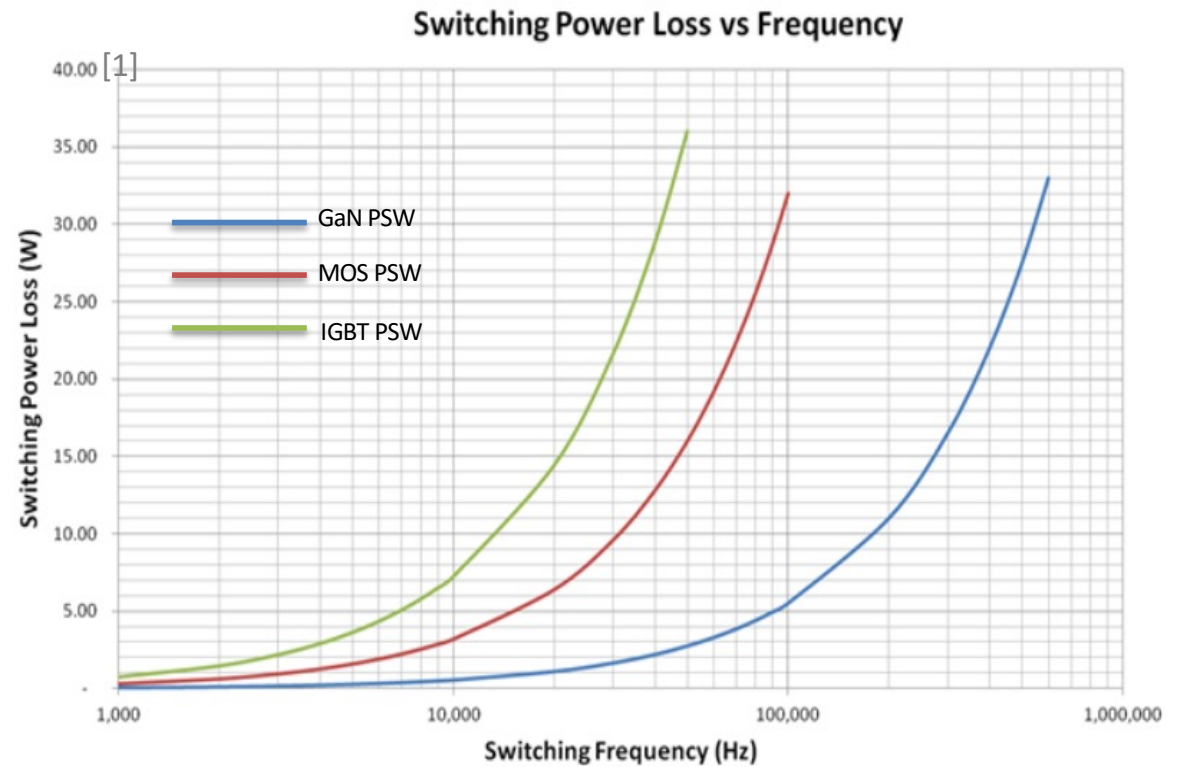


Switching losses are proportional to the switching frequency...

...while conduction losses are fixed

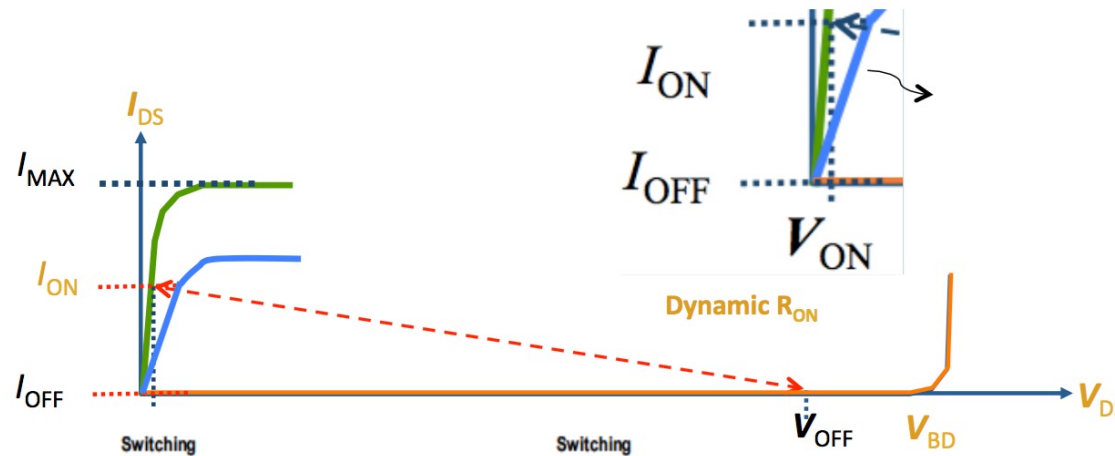


(c) Comparison of switching properties of Si-IGBT and GaN-HEMT



Switching losses are proportional to the switching frequency: Fast devices are required!

## Power switch:

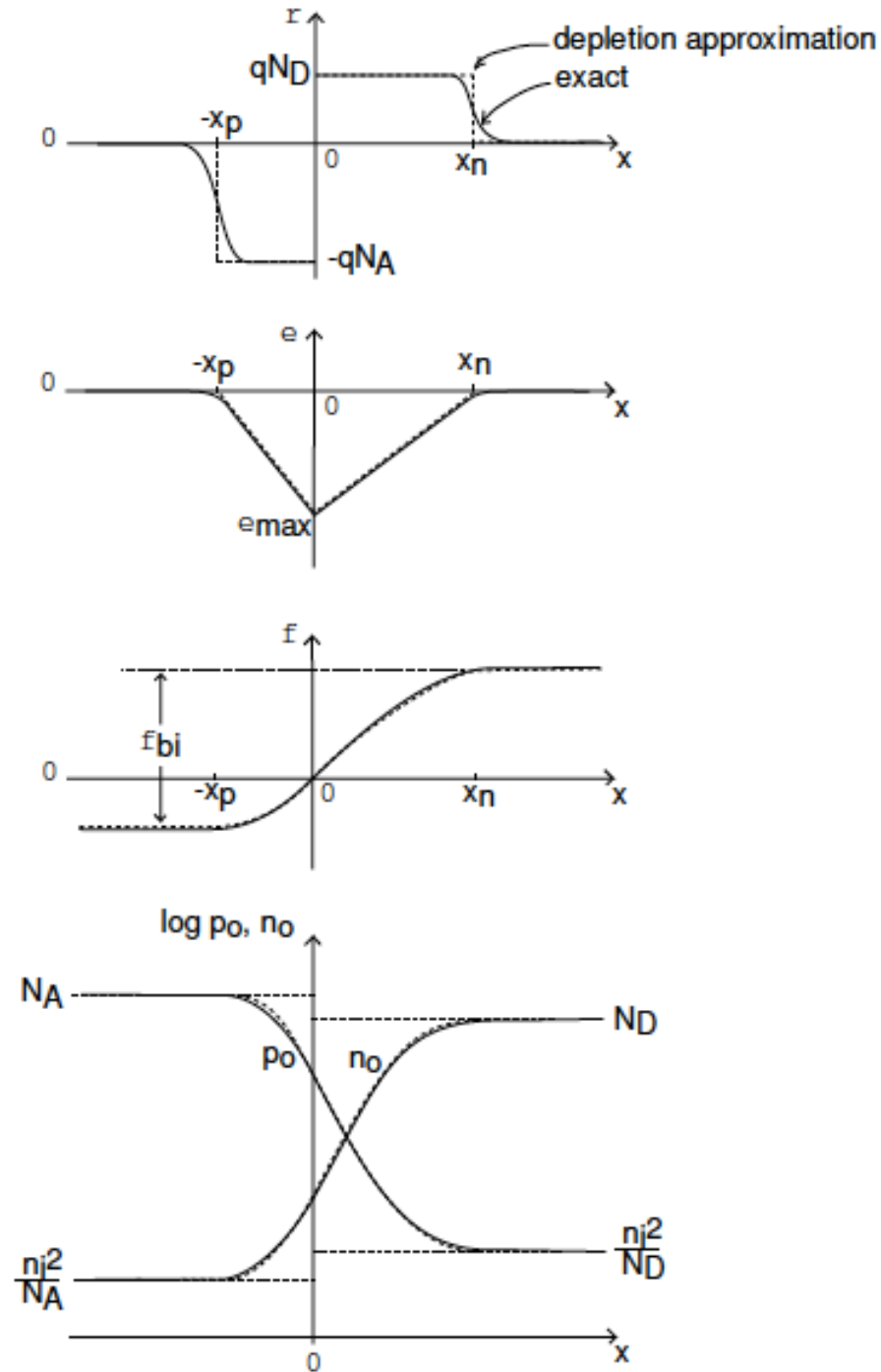
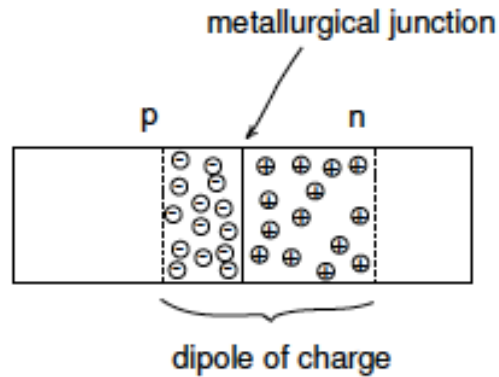


It operates in two regimes:  
 ON: Low voltage, high current  
 OFF: High voltage, low current

- High breakdown voltage
- Low on-resistance: Small on-state power dissipation:  $I_{rms}^2 \times R_{on}$
- High maximum current
- Low leakage current at breakdown voltage: Small off-state power dissipation:  $I_{off} \times V_{br}$

**How to get large breakdown voltages?**

# Back to pn junctions



## Distinct regions:

Around metallurgical junction:  
**space charge region (SCR)**

Far from junction:

**quasi-neutral regions (QNR)**

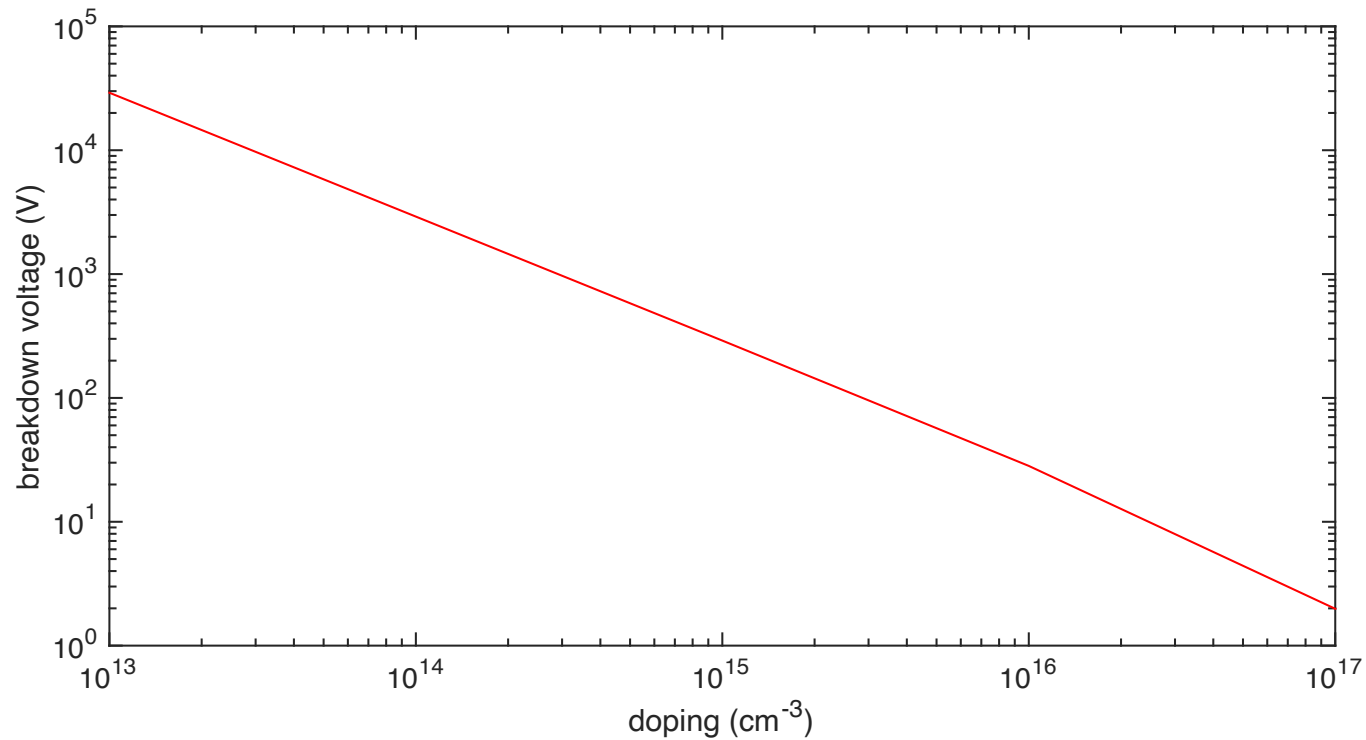
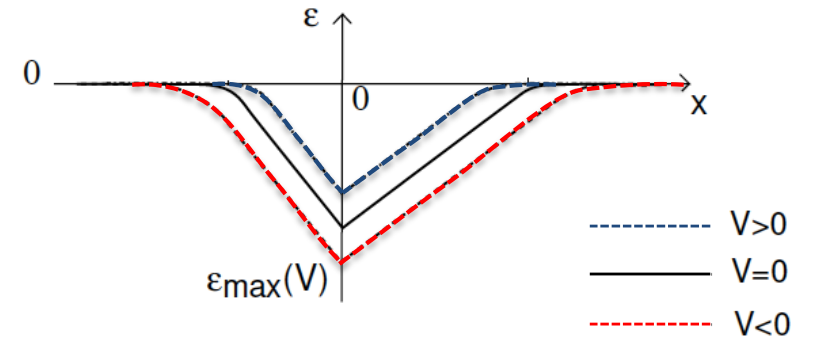
$$\rho \sim 0$$

Electric field is constant and equal to zero

# Ideal p-n junction out of equilibrium

Peak electric field:

$$|\mathcal{E}_{max}(V)| = \sqrt{\frac{2qN_A N_D (\phi_{bi} - V)}{\epsilon(N_D + N_A)}} = |\mathcal{E}_{max}(V = 0)| \sqrt{1 - \frac{V}{\phi_{bi}}}$$



How to make a power device?

Goal:

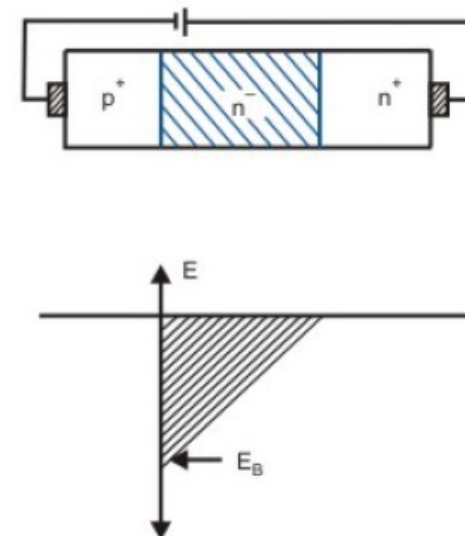
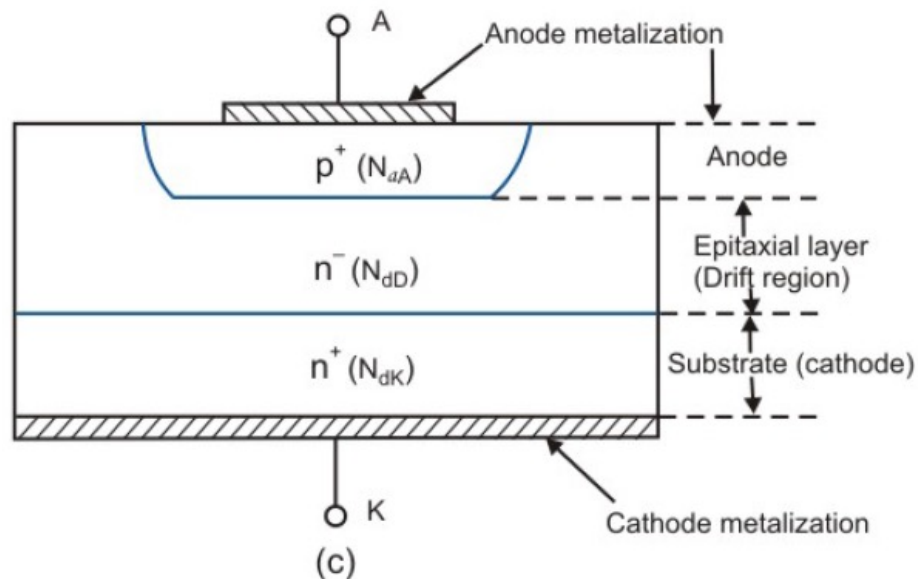
Conduct **several kilo amps** of current in the forward direction with very **little power loss** while blocking **several kilo volts** in the reverse direction.

**Large blocking voltage** requires **wide depletion layer** in order to restrict the maximum electric field strength below the breakdown voltage (impact ionization level).

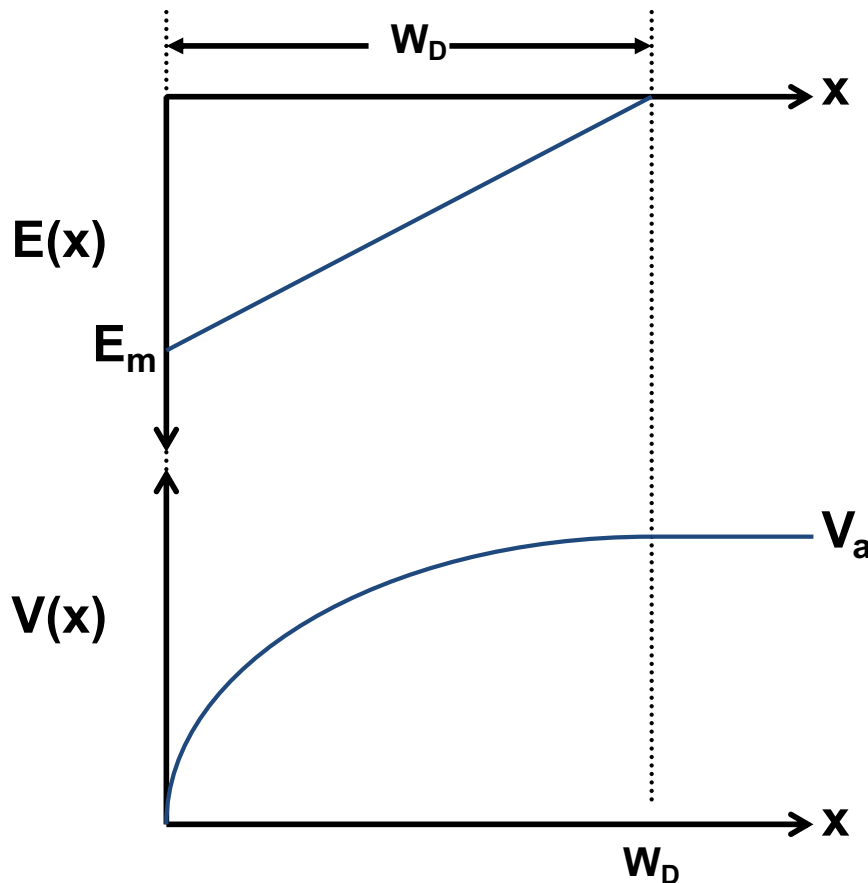
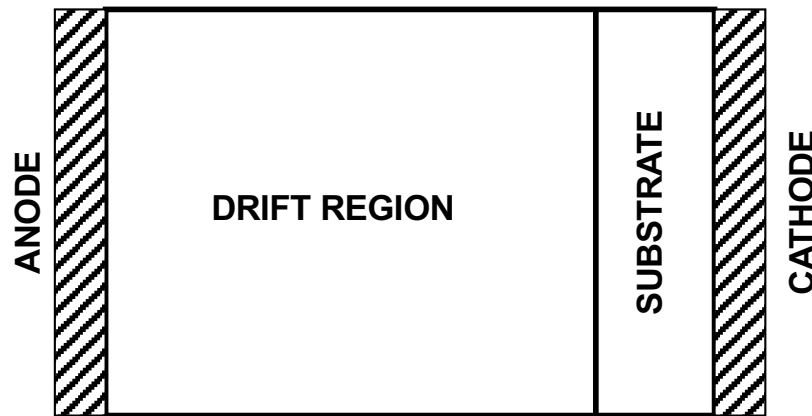
Space **charge density in the depletion layer should also be low** in order to yield a wide depletion layer for a given **maximum electric field strength**.

This is satisfied in a **lightly doped p-n junction diode of sufficient width** to accommodate the required depletion layer.

## PIN diode



# Figure of merit: how to compare different semiconductors



Specific on-resistance ( $\Omega\text{cm}^2$ )

$$R_{\text{ON,SP}} = \frac{W_D}{qN_D\mu_n}$$

$$V = \frac{E_m W_D}{2} \quad \text{thus} \quad \boxed{W_D = \frac{2BV}{E_C}}$$

Poisson's Equation:

$$\frac{d^2V}{dx^2} = -\frac{dE}{dx} = -\frac{Q(x)}{\epsilon_S} = -\frac{qN_D}{\epsilon_S}$$

$$E(x) = -\frac{qN_D}{\epsilon_S} (W_D - x)$$

$$V(x) = \frac{qN_D}{\epsilon_S} \left( W_D x - \frac{x^2}{2} \right)$$

$$V_a = \frac{qN_D W_D^2}{2\epsilon_S}$$

$$\boxed{N_D = \frac{\epsilon_S E_C^2}{2qBV}}$$

**Ideal Specific On-Resistance ( $R_{ON,SP}$ ):**

$$W_D = \frac{2BV}{E_C} \quad \text{and} \quad N_D = \frac{\epsilon_S E_C^2}{2qBV}$$

$$R_{ON,SP} = \frac{W_D}{q\mu_n N_D}$$

$$R_{ON,SP} = \frac{4BV^2}{\epsilon_S \mu_n E_C^3}$$

$R_{on,sp}$  is related to material properties

**Baliga's figure of merit**

$$BFOM = \epsilon_S \mu_n E_C^3 = \frac{4BV^2}{R_{ON,SP}}$$

Critical electric field  $E_c$  is very important, followed by mobility in the drift layer

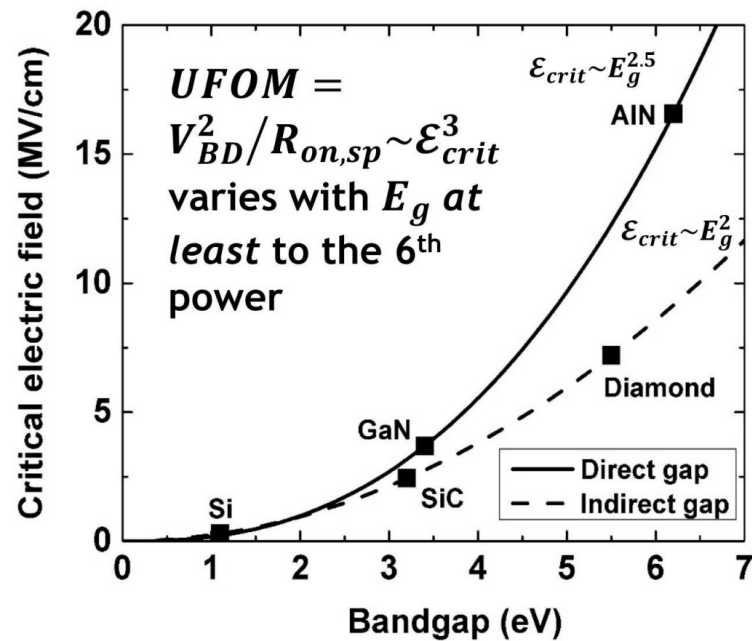
$$R_{ON,SP} = \frac{4BV^2}{\epsilon_S \mu_n E_C^3}$$

$R_{on,sp}$  is related to material properties

Baliga's figure of merit

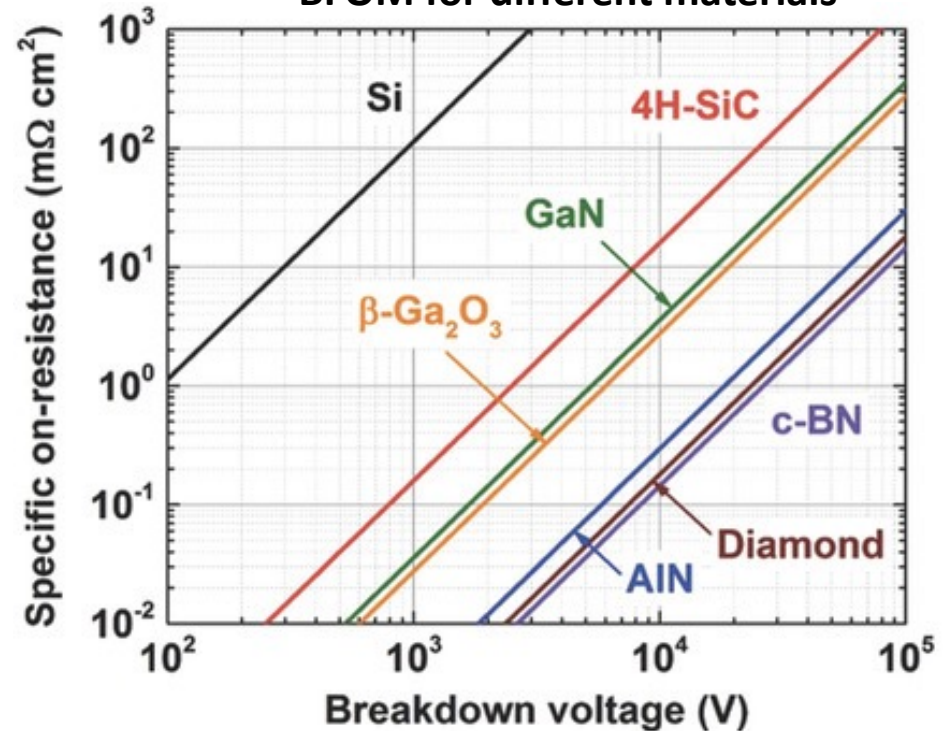
$$BFOM = \epsilon_S \mu_n E_C^3 = \frac{4BV^2}{R_{ON,SP}}$$

Relationship between  $E_c$  and  $E_g$



Hudgins et al., IEEE Trans. on Pow. Elec. 18, 3 (2003),  
Tsao et al., Advanced Elec. Mat. 4, 1600501 (2018)

BFOM for different materials



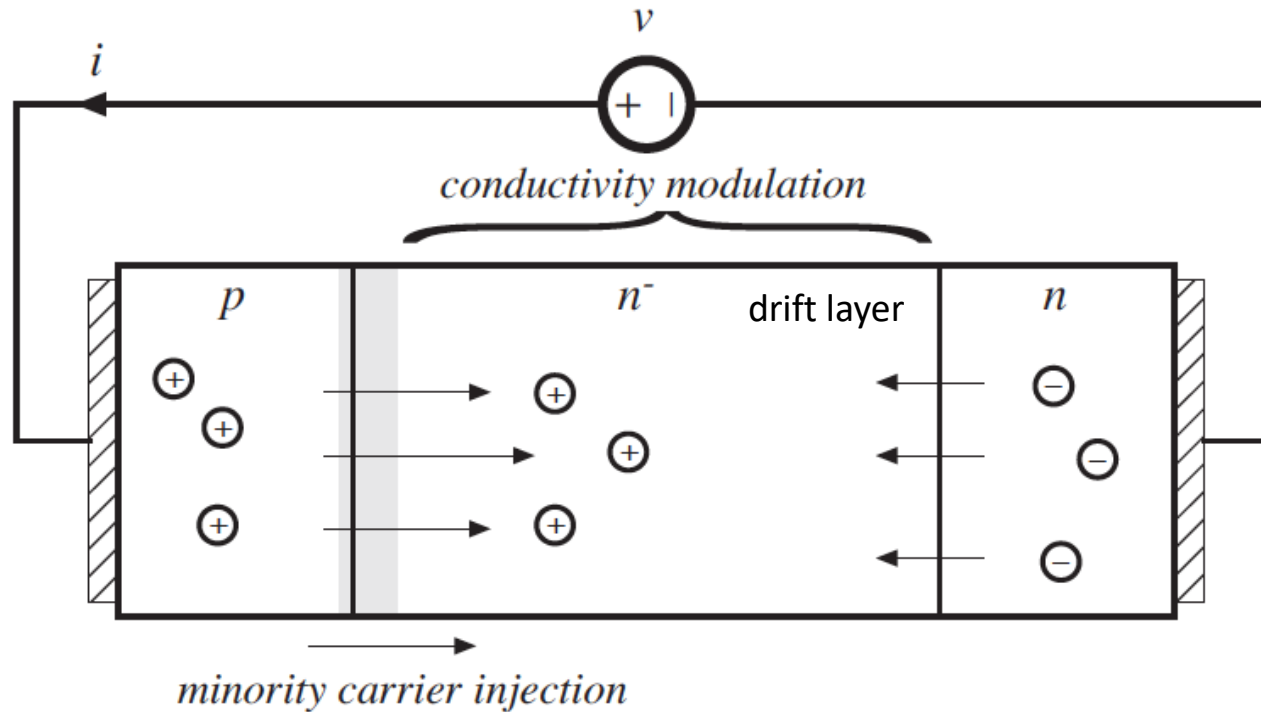
Parameter	Silicon	4H-SiC	GaN	Diamond
$E_g$ , eV	1.12	3.26	3.39	5.47
$E_{crit}$ , MV/cm	0.23	2.2	3.3	5.6
$\epsilon_r$	11.8	9.7	9.0	5.7
$\mu_n$ , cm <sup>2</sup> /V·s	1400	950	800/1700 <sup>b</sup>	1800
BFoM <sup>a</sup> relative to Si	1	500	1300/2700 <sup>b</sup>	9000
$n_i$ , cm <sup>-3</sup>	$1 \cdot 10^{10}$	$8 \cdot 10^{-9}$	$2 \cdot 10^{-10}$	$1 \cdot 10^{-20}$
$\lambda$ , W/cm·K	1.5	3.8	1.3/3 <sup>c</sup>	20

Desired properties, found in some of these wide band-gap materials:

- Higher breakdown strength: same breakdown voltage with less material
- Higher switching speed: lower switching losses
- Lower losses: enables significantly reduced volume and decreased cooling requirements
- Higher frequency: smaller passive components (inductors and capacitors)

diode PIN

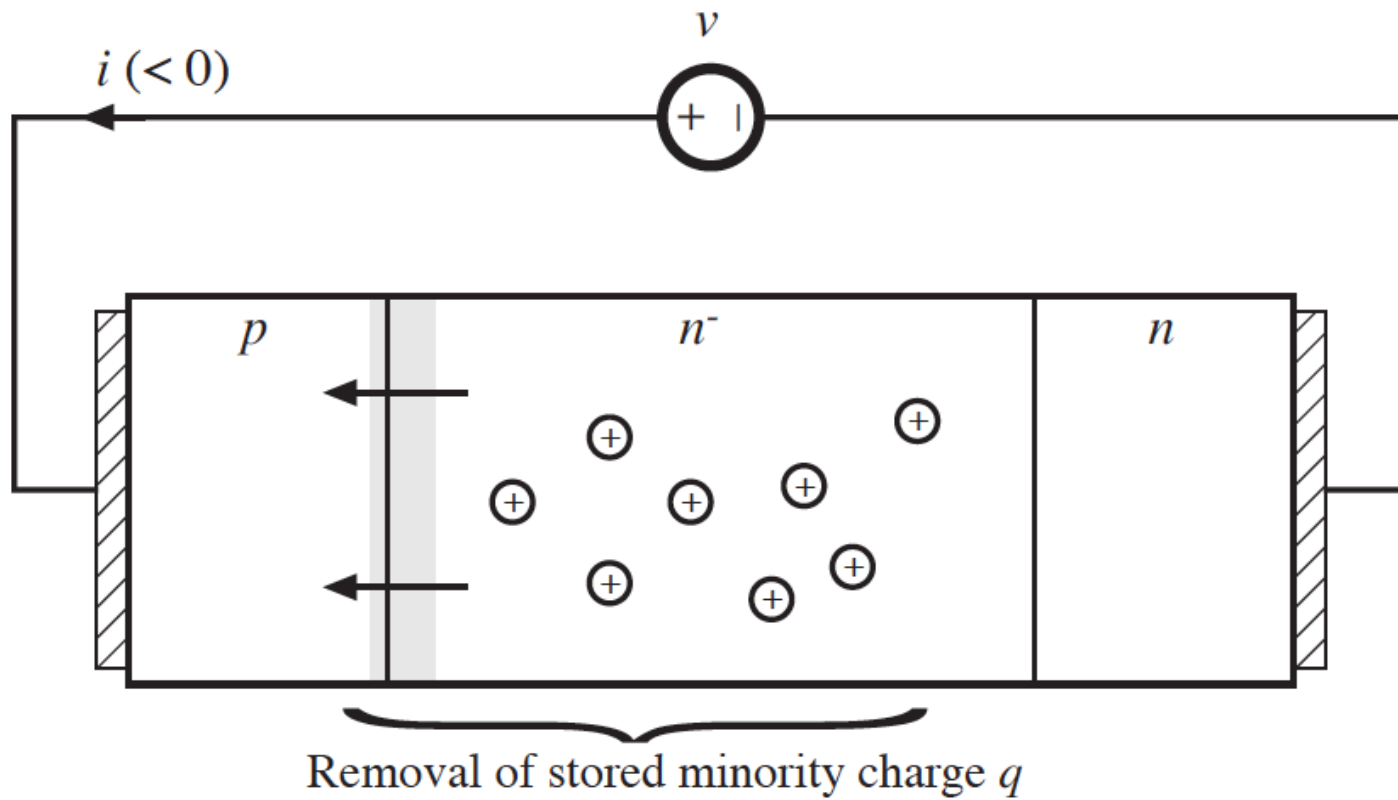
Forward polarization

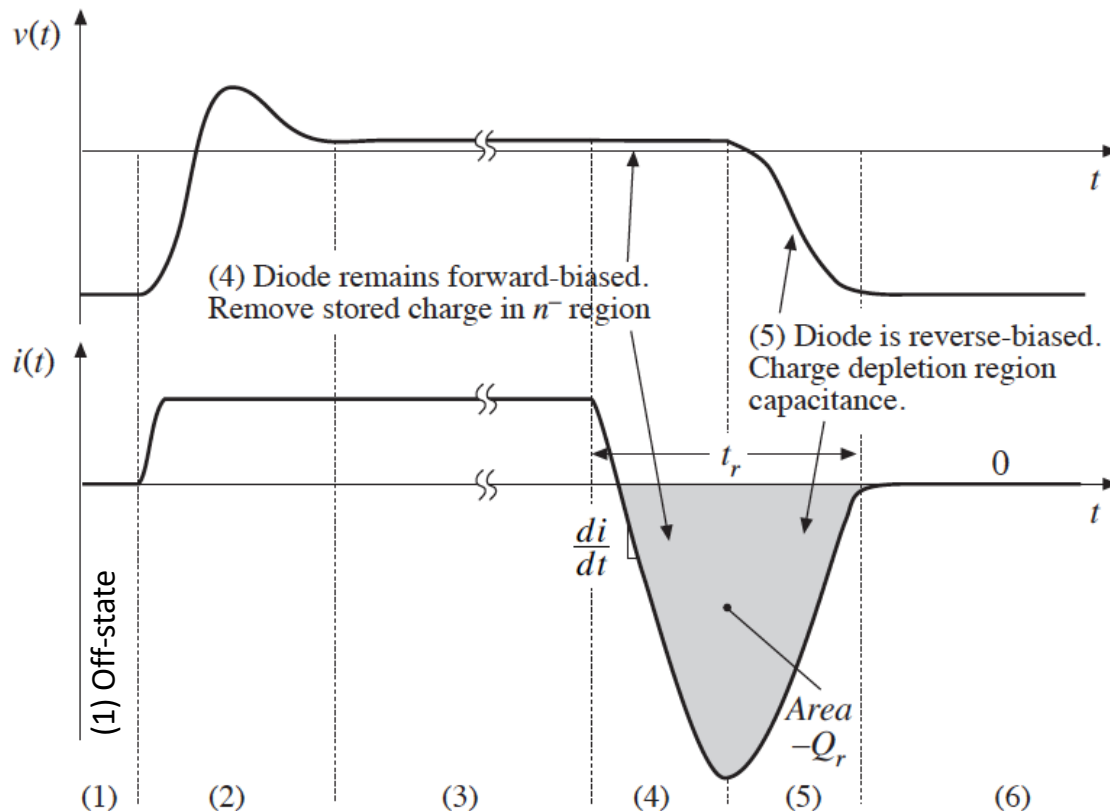


Forward polarization:

- Injection of minority carriers in the drift layer: conductivity modulation
- Charges are accumulated in the region «i»:
  - Resistance is reduced
  - But slows down the device
- Minority carrier device

Turn-off transient





(4) Reduction of the stored minority charge can be accomplished either by active means, via **negative terminal current**, or by passive means, via **recombination**. Normally, both mechanisms occur simultaneously.

The charge contained in the negative portion of the diode turn-off current waveform is called the **recovered charge**.

Minority charges are actively-removed during interval (4).

At the end of interval (4), the stored minority charge in the vicinity of the **junction has been removed**, such that the diode junction becomes **reverse-biased** and is able to **block negative voltage**.

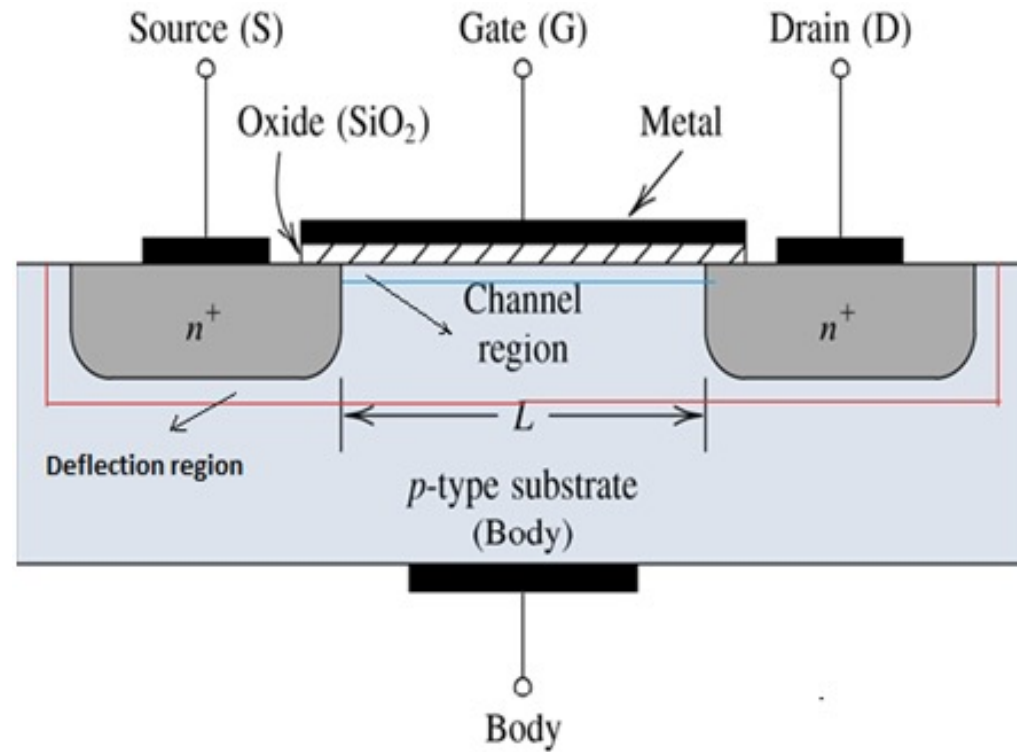
The depletion region **effective capacitance is then charged** during interval (5) to the negative off-state voltage.

The portion of  $Q$  during interval (5) is **charge supplied to the depletion region**, as well as minority charge that is actively removed from remote areas of the diode.

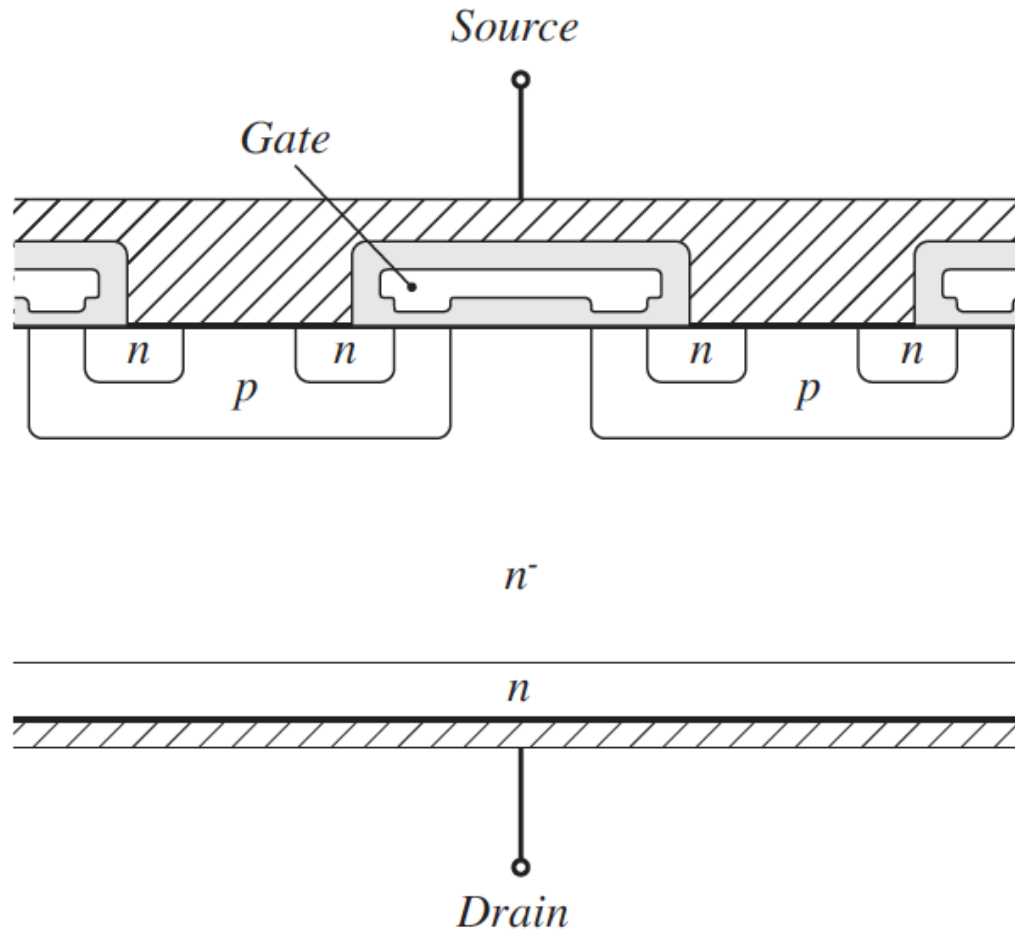
At **the end of interval (5)**, the diode is able to **block the entire applied reverse voltage**.

The length of intervals (4) and (5) is the **reverse recovery time  $t_r$** .

**$Q_r$ : reverse recovery charges: diode is very slow!**

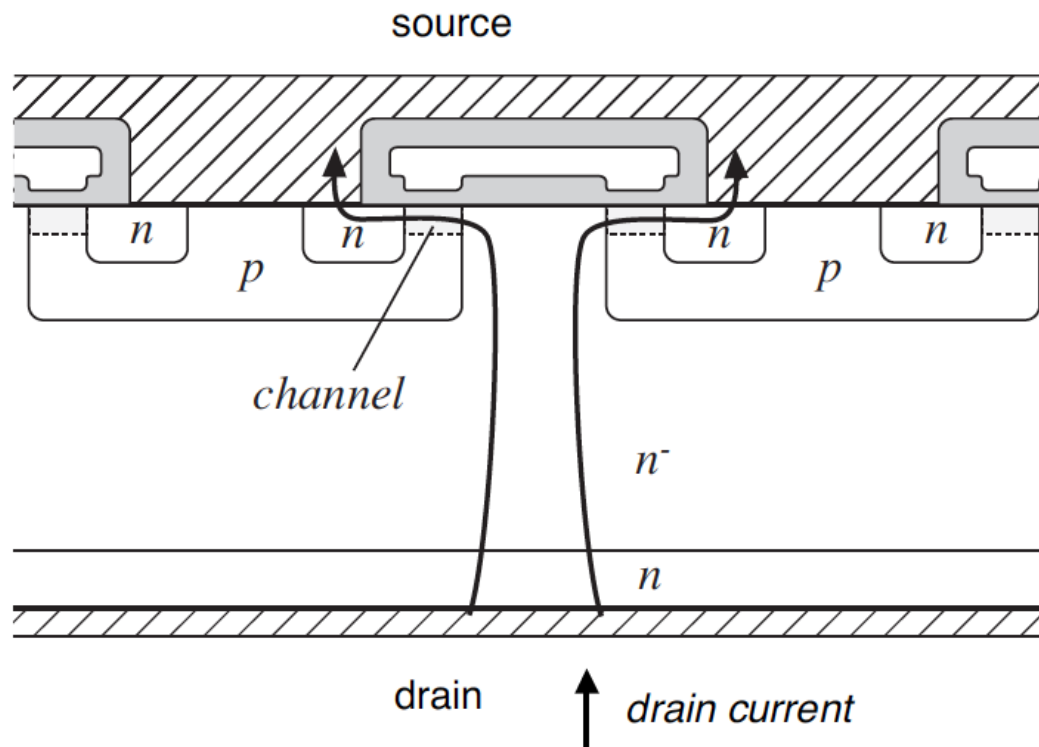


**How to make a power MOSFET?**



- Gate lengths approaching one micron
- Consists of many small enhancement-mode parallel-connected MOSFET cells, covering the surface of the silicon wafer
- Vertical current flow
- n-channel device is shown

Forward polarization:  $V_{gs} > 0$

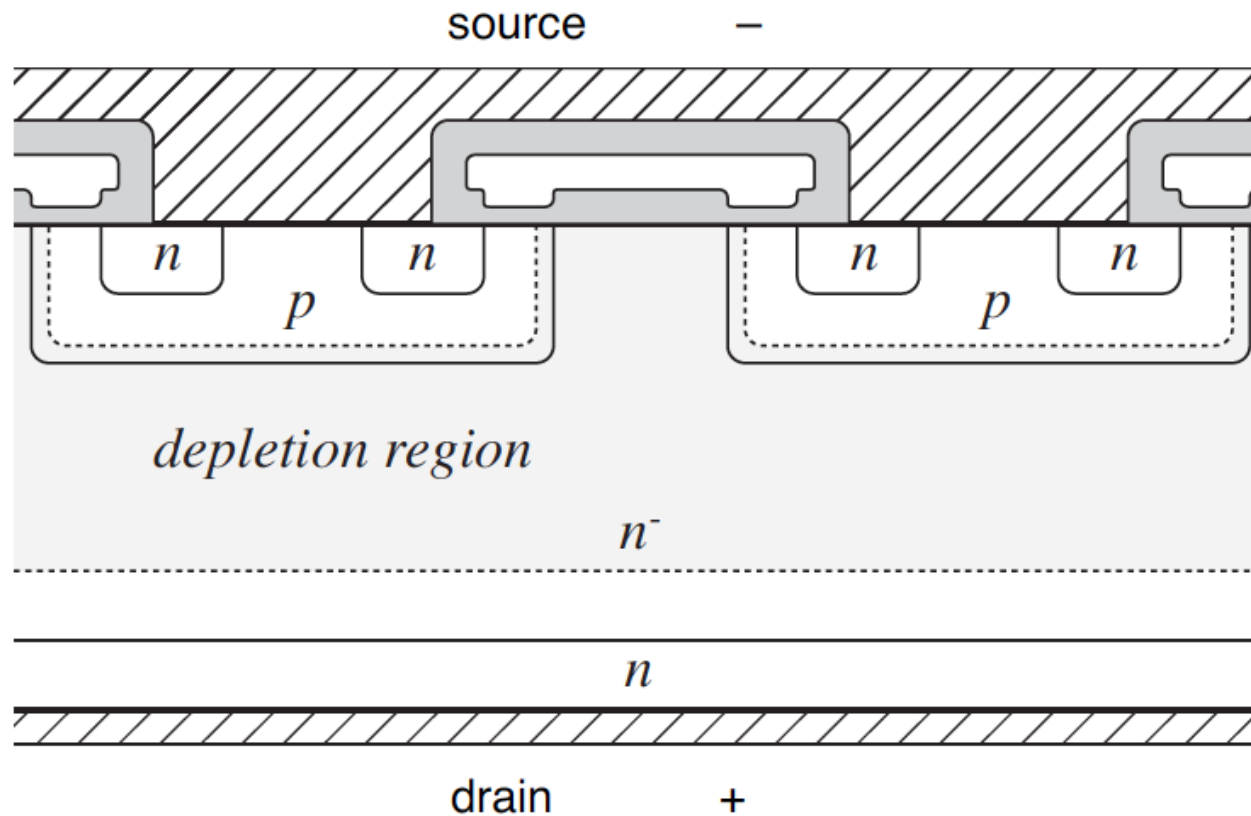


- $p$ - $n$  junction is slightly reverse-biased
- positive gate voltage induces conducting channel
- drain current flows through  $n^-$  region and conducting channel
- on resistance = total resistances of  $n^-$  region, conducting channel, source and drain contacts, etc.

There are no minority carriers to cause conductivity modulation: **MOSFETs are majority carrier devices**

- Breakdown voltage is increased
- On-resistance dominated by resistance of  $n^-$  region.

Reverse polarization:  $V_{gs} < 0$

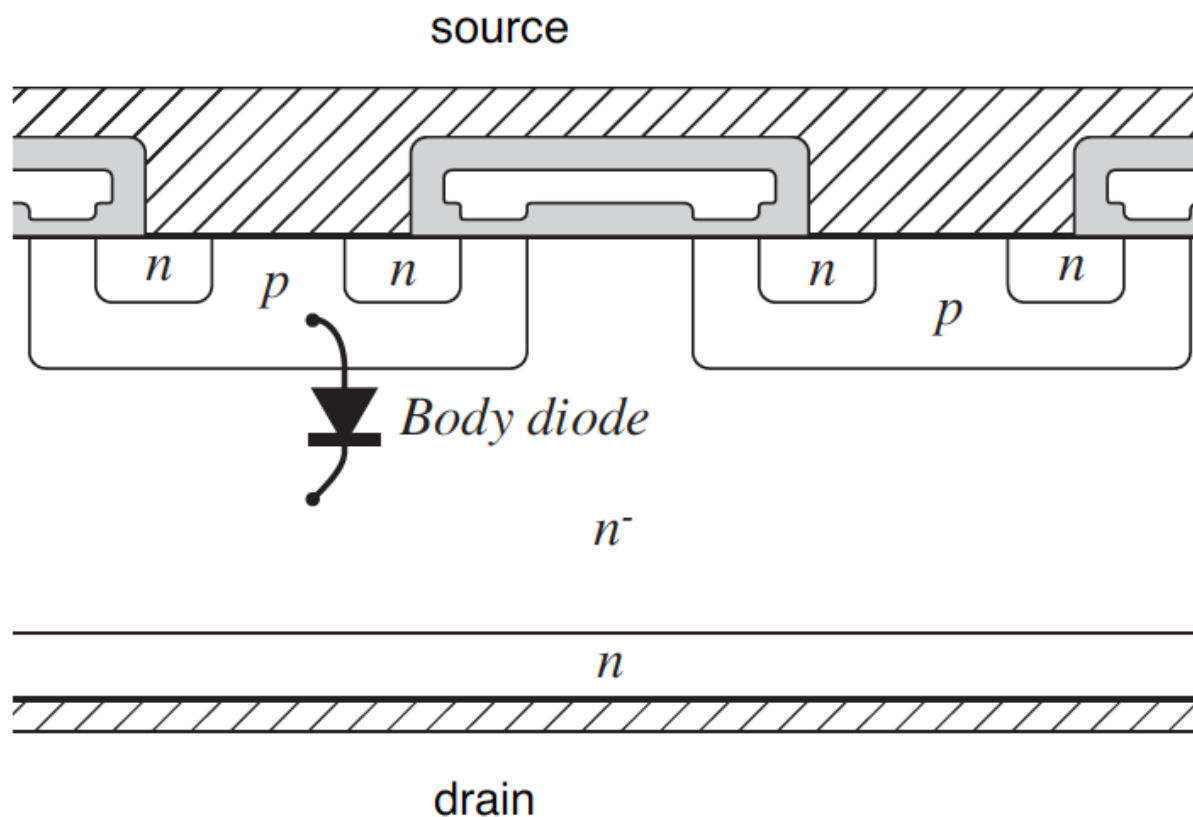


- $p-n^-$  junction is reverse-biased
- off-state voltage appears across  $n^-$  region

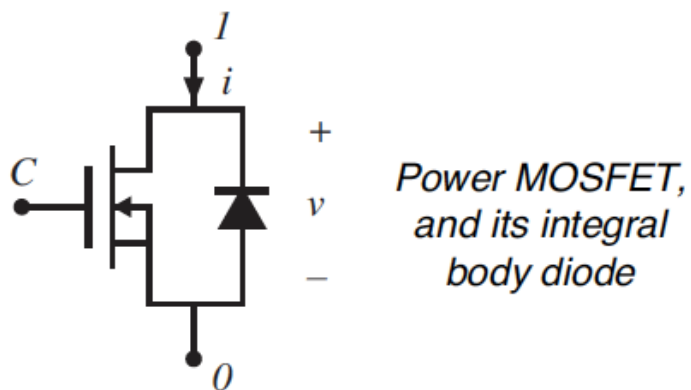
**Polarisation reverse:**

$p-n$  and  $p-n^-$  reverse-biased: voltage drops across  $n^-$  region

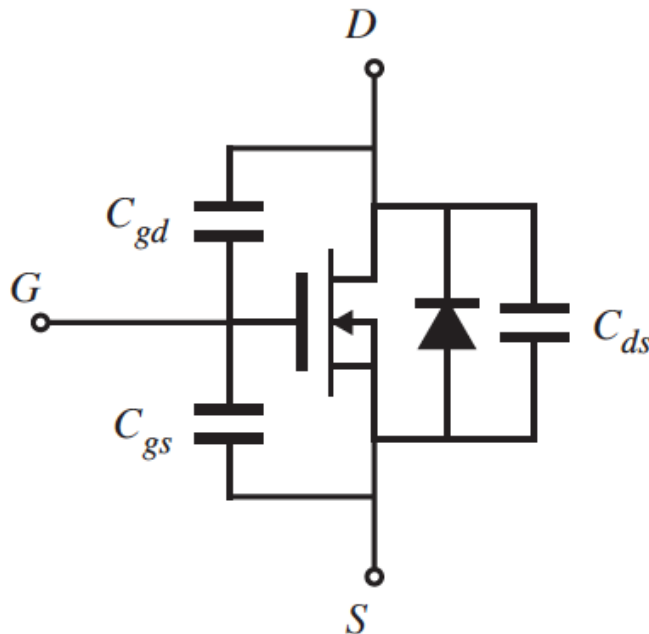
## MOSFET: body-diode



- $p-n$  junction forms an effective diode, in parallel with the channel
- negative drain-to-source voltage can forward-bias the body diode
- diode can conduct the full MOSFET rated current
- diode switching speed not optimized — body diode is slow,  $Q_r$  is large



## MOSFET: equivalent circuit



- $C_{gs}$  : large, essentially constant
- $C_{gd}$  : small, highly nonlinear
- $C_{ds}$  : intermediate in value, highly nonlinear
- switching times determined by rate at which gate driver charges/discharges  $C_{gs}$  and  $C_{gd}$

$$C_{ds}(v_{ds}) = \frac{C_0}{\sqrt{1 + \frac{v_{ds}}{V_0}}}$$

$$C_{ds}(v_{ds}) \approx C_0 \sqrt{\frac{V_0}{v_{ds}}} = \frac{C'_0}{\sqrt{v_{ds}}}$$

$C_{gd}$  is small but the voltage is large: so a lot of charges stored